# Montana Department of Transportation Research Program August 2007

### EXPERIMENTAL EVALUATION REPORT

## **Thin-Whitetopping Bonded Composite**



Location: Glendive, Montana – Dawson County

Project No.: STPP 20-1(6)0, P-20, C000020; Highway 16, Milepost 0-0.6

FHWA No. MT 00-04

Description: Sixth year analysis of experimental thin-whitetopping (TW)

construction project consisting of milling approximately 38mm of Asphalt Cement (AC) and placement of 100mm Portland Cement (PCCP) onto the milled surface to create a bonded, composite

pavement. Project length-0.9 kilometer (0.6 mile).

Date of Evaluation: August 2007

Date Constructed: May 2001

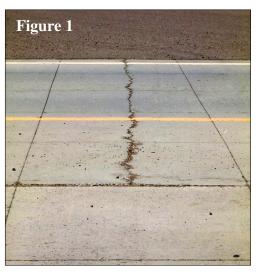
Report Origin: Craig Abernathy

Experimental Project Manager

## **Purpose**

Highway 16 (P-20) suffered from rutting, plastic deformation and transverse cracking. The Montana Department of Transportation decided to construct a thin-whitetopping project based on minor rehabilitation criteria. Whitetopping is an alternative to the regular program of mill & fill. This procedure bonds a flexible layer to a rigid layer to form a bonded composite pavement, which eliminates rutting and plastic deformation. Currently, the Department considers this type of pavement treatment experimental. This project will be formally evaluated for the duration of the life of the whitetopping.

### **Documentation**



A visual inspection of the entire project was performed to document all types of surface cracking and distress. Photographic documentation of some of the cracks, recent repairs, as well as a representative crack map is included in this report. Note that the crack map is strictly an interpretation of progressive distress during the evaluation phase of the project, it is not to scale. Currently three transverse cracks are present on this project, all in the southbound lane. Location as follows (footage counted from the south end of the project going north), #1 at 1244' (541m), #2 at 1380' (420m), and #3 at 1480' (451m), see crack map at end of report. Note that these cracks developed soon after placement

during construction. These cracks have widened since construction and are rated as severe in nature (example of crack in figure 1). Incompressible debris (rocks, friables etc,) is entering the cracks and will accelerate the deterioration of the fracture with freeze thaw events, however no debonding of the asphalt and PCCP layer was observed with any of the existing transverse cracks in this evaluation. No additional transverse cracking has occurred since construction.



A total of approximately eighteen panels have cracked since construction. A cracked panel does not necessarily mean a failure of the bond between the AC and PCCP layers. To date, no panel movement or

deflection was noticed on any of the panels as traffic moved over them.

Fifteen panels were affected at the north and south end of the project on the southbound lane. In fall of 2005 both these areas were repaired due to the extent of the panel cracking. The repair involved removal of the existing PCCP and asphalt layers and replaced with full-depth PCCP.



During this analysis several more panels have cracked, located at the north edge of the southbound lane of the project; adjacent to the recent full-depth repair (figure 2, crack panel shown as black line in image). In this type of cracking which

is indicative of this kind of pavement treatment, without an autopsy of the panel, it is difficult to determine the various causes of cracking. It could entail debonding of the PCCP from the asphalt concrete, structural failure of the underlying AC layer, which visually, has not been seen, or possibly overloading of the composite panel or sympathy cracking. In addition, panels that have previously cracked are at or near the curb edge adjacent to areas where turning movements of heavy trucks are traveling onto the gravel curb and onto the edge of the PCCP pavement. The lack of support may have allowed



cracking at these locations (refer to the crack map at the end of this document). Figure 3 (located midway on southbound side) shows how the lack of curb supports can allow panels to crack from heavy loadings. Though not apparent in this photograph the south adjacent panel has also cracked and will continue to degenerate.

The current Ride Index for the northbound lane is rated at 200 and for the southbound lane at 178, both grouped as being in the 'poor' ride category. The northbound lane is rougher than the southbound.

This may have been caused by the type of paver that was used during construction. The contractor used an old style, Alan three-tube paver; which could have inadvertently (due to the back and forth action of the unit) created the undulation or 'rough ride' as indicated. In addition, since the paver rested on the east edge of the previously placed southbound

lane during construction, it most likely accelerated the roughness aspect of the ride for the northbound lane.

Several areas on the project are showing signs of wear and tear with slight spalling at panel saw cuts, to date minimum occurrences but gradually appearing. Figure 4 is an example of the spalling.

Regardless of the ride analysis and accumulative cracking to date. The next evaluation will be held in the summer of 2008

